Reactivation of aged model $Pd/Ce_{0.68}Zr_{0.32}O_2$ three-way catalyst by high temperature oxidising treatment[†]

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A deactivated (aged under redox-cycled model TWC feedstream) Pd/Ce_{0.68}Zr_{0.32}O₂ catalyst is remarkably reactivated when subjected to a high temperature oxidising treatment whereas this effect is only marginal for Pd/Al₂O₃, which indicates the key role of such treatment in restoring the Pd– Ce_{0.68}Zr_{0.32}O₂ interactions leading to highly active catalysts.

Extremely demanding limits for durability (life-time up to 120 000 miles, equivalent to 10 years' vehicle use) and activity (conversion over 98%) have been set up by US TIER2 and European legislation on the abatement of automotive pollution. The state of the art automotive three-way catalysts (TWCs) contain NMs (noble metals: Pt, Rh and Pd) supported on high surface area CeO2-ZrO2 mixed oxides and Al2O3; which are in turn supported on honeycomb-type supports.1 These systems show very high catalytic efficiency when fresh, whereas the issue of deactivation has received relatively scant attention. Catalyst poisoning due to Zn and P contained in the engine oil and thermal sintering of Al₂O₃, CeO₂-ZrO₂ and the supported metal particles represent the major pathways for the deactivation processes.^{2,3} Thermally stable CeO₂-ZrO₂-Al₂O₃ composites have been suggested as a suitable way for preventing sintering of these components.^{4,5} In contrast indications of how to efficiently prevent NM sintering are missing. Accordingly, strategies to stabilise nano-dispersed metal particles have been extensively investigated.^{6,7} Here we show that a high temperature oxidative treatment of an aged Pd/Ce_{0.68}Zr_{0.32}O₂ is capable of restoring activity levels comparable to the fresh catalyst. This effect is particularly noticeable because the aging induces a strong sintering of the catalyst. The use of $Ce_{0.68}Zr_{0.32}O_2$ as support plays a fundamental role in this mechanism.

Pd 0.64 wt%/Ce_{0.68}Zr_{0.32}O₂ (BET surface area 104 m² g⁻¹) indicated as PdCZ Fresh, was supplied by Rhodia. A reference Pd 0.51 wt%/Al2O3 (BET surface area 148 m² g⁻¹) catalyst was also employed. Catalytic tests and ageing treatments were performed using model exhaust oxidising and reducing mixtures: C₃H₆, 900 ppm; NO, 900 ppm; CO₂, 10%; H₂O, 10% and N₂ to balance; CO, 1.6% and O₂, 0.465% were employed for the reducing mixture (airto-fuel (A/F) = 14.13); CO, 0.4% and O_2 , 1.26% for the oxidizing mixture (A/F = 15.17). Notice that A/F = 14.63 at stoichiometry. The accelerated ageing procedure8 was performed by heating at 8 K min-1 from 373 to 1173 K and ageing for 5 hours at 1173 K under the above quoted model exhaust mixtures using a cycling frequency of 0.0055 Hz. The samples were cooled to 423 K either under the cycled feedstream (cycling frequency of 0.0167 Hz) (sample Aged-Cyc) or under the oxidising reaction mixture (sample Aged-Ox) and then to room temperature in N2 flow. The ageing conditions, 1173 K under a redox cycling mixture, were chosen to ensure strong sintering of both Pd and Ce_{0.68}Zr_{0.32}O₂ support while avoiding extensive NM encapsulation.9 Before testing, the catalysts were reduced for 1 hour at 573 K in a H₂ (5%)/N₂ flow. Light-off experiments were conducted under cycled conditions (1 Hz) using a space velocity of 125 000 h⁻¹. Dynamic oxygen storage and release capacity using CO as reducing agent (CO-OSC) was measured as reported previously.¹⁰ H₂O (10%) was added to the carrier gas flow (Ar) through a saturator at 319 K. HREM, SEM-EDS, temperature programmed desorption, reduction and oxidation (TPD, TPR, TPO), XRD and CO and H₂ chemisorption studies were performed as already described.^{4,11}

The effects of ageing procedures on PdCZ and Pd/Al₂O₃ are summarised in Table 1. Despite the fact that an equal degree of sintering was experienced by the PdCZ catalysts (BET area drops from 104 m² g⁻¹ (fresh) to 30 m² g⁻¹ in both Aged-Cyc and Aged-Ox) and equal pre-treatment (reduction at 573 K), there is a remarkable difference in terms of catalytic efficiency of the two aged catalysts: PdCZ Aged-Ox features a conversion efficiency that is comparable to that of PdCZ-Fresh.

Both TPD and TPO experiments performed on the PdCZ Aged-Cyc and Aged-Ox samples revealed evolution of traces of adsorbed H₂O and CO₂ consistent only with some unavoidable sample contamination upon exposure to air. This rules out the presence of surface carbonaceous residuals as responsible for the deactivation of the PdCZ Aged-Cyc compared to Aged-Ox. Noteworthy is the decrease of CO and O₂ conversion efficiency induced by the Aged-Cyc procedure which leads to an increase of light-off (50% conversion) temperature, T_{50} , by about 150–160 K compared to Aged-Ox. Re-oxidation of the Aged-Cyc PdCZ at 1173 K leads to significant recovery of the activity, indicating the crucial role of the final oxidising part of the ageing procedure in preventing the deactivation. Only a minor difference in the activity with the ageing procedure was found for a Pd/Al₂O₃ catalyst, which indicates the critical role of the $Ce_{0.68}Zr_{0.32}O_2$ support in favouring this unexpected regeneration of the catalyst induced by the "Ox" part of the ageing procedure.

A bifunctional reaction mechanism is typically invoked for the NM/CeO2-based catalysts where the activity of the NM is promoted by the support, and particularly by its highly efficient redox capability (OSC).12 Dynamic CO-OSC was measured (Fig. 1, Table 1) to assess the effects of the support. It shows that: i) CO-OSC, *i.e.* "support mediated" CO oxidation by O₂, is marginally affected by addition of water whereas occurrence of water gas shift reaction (WGSR) was detected, as revealed by concurrent H₂ production; ii) both CO-OSC and WGSR occur only to a small extent over PdCZ Aged-Cyc, iii) high CO-OSC/WGSR activity is observed over the PdCZ Aged-Ox; and remarkably iv) high temperature oxidation (1173 K) of PdCZ Aged-Cyc restores high activity in both CO-OSC and WGSR. Thus these data confirm that the "Ox" treatment has restored the promoting capabilities of the Ce_{0.68}Zr_{0.32}O₂ support. Consistently, HREM revealed a statistically significant difference between Aged-Ox and Aged-Cyc Ce_{0.68}Zr_{0.32}O₂ nanocrystal morphology (Fig. 2). Sharply defined nano-facets are typically found in Aged-Cyc whereas rounded, less-faceted morphology was detected in Aged-Ox sample. No Pd particles could be detected by HREM.

196

Chem. Commun., 2004, 196-197

Table 1 Effects of ageing procedures on the light-off temperature, T_{50} , for CO, NO and C_3H_6 conversion, CO-OSC, BET surface areas and chemisorption properties of Pd/Ce_{0.68}Zr_{0.32}O₂ and Pd/Al₂O₃ catalysts.

	T ₅₀ / K			Dynamic CO-OSC ^a (without H ₂ O)			
Catalyst	СО	NO	C ₃ H ₆	O ₂ uptake/ml g ⁻¹	$m^2 g^{-1}$	H/Pd^b	CO/Pd ^b
PdCZ Fresh	406	549	523	6.3 (7.1)	104	9.1	0.64
PdCZ Aged-Ox	413	541	530	4.1 (3.5)	30	1.1	0.14
PdCZ Aged-Cyc	588	628	598	1.8	30	0.10	0.06
PdCZ Aged-Cyc-Ox ^c	508	610	540	4.1			
PdAl Aged-Ox	567	584	569	< 0.4	123	0.09	0.08
PdAl Aged-Cyc	589	608	588	< 0.4	119	0.03	0.04

^{*a*} CO-OSC measured as O_2 uptake at 573 K. Note that non stoichiometric values of CO_2 produced/CO consumed in comparison to O_2 consumed were observed in the presence of H_2O due to concurrent H_2 formation *via* WGSR. H_2 production was confirmed by MS (Fig. 1). For comparison O_2 uptakes of 0.9 and < 0.4 ml g⁻¹ are observed respectively over fresh $Ce_{0.68}Zr_{0.32}O_2$ and Pd/Al_2O_3 . An uptake of 0.5 ml O_2 g⁻¹ is calculated for the Pd/PdO redox process assuming that all Pd is involved. Standard deviation 0.4 ml O_2 g⁻¹. ^{*b*} Sample reduced at 573 K; measured in the range of pressures 2–20 torr to minimize formation of Pd hydride and CO adsorption on the support; almost no CO_2 evolution was detected following the O_2 pulse in the CO-OSC experiments over these samples in agreement with negligible CO adsorption over the support. ^{*c*} Sample oxidized at 1173 K for 15 min in the oxidizing mixture and then cooled to 423 K in the same mixture or (CO-OSC) oxidized by pulses of O_2 (250 µl every 70 s) at 1173 K for 5 h and then cooled under O_2 pulses.



Fig. 1 Effect of H₂O addition and ageing procedures on dynamic CO-OSC at 673 K over Pd/Ce_{0.68}Zr_{0.32}O₂: (a) Aged-Ox in the absence of H₂O, (b) Aged-Ox in the presence of H₂O, (c) Aged-Cyc in the presence of H₂O, (d) Aged-Cyc-Ox (sample Aged-Cyc from experiment (d) oxidized *in situ* at 1173 K) in the presence of H₂O, (e) Aged-Cyc-Ox in the absence of H₂O, (f) Aged-Cyc-Ox in the presence of H₂O. The tailing of peaks in (b)–(d) is due to H₂ evolution (WGSR) that occurs under the CO and CO₂ peaks, as revealed by the MS traces (compare (e)–(f)).



Fig. 2 HREM micrograph of Pd/ $Ce_{0.68}Zr_{0.32}O_2$: (A) Aged-Cyc and (B) Aged-Ox. In the insets DPP patterns showing the presence of *t*-phase.

Pd redispersion¹³ over the support, induced by the "Ox" treatment that affects the delicate – support-dependent – PdO/Pd equilibrium,¹⁴ can be invoked as one of the factors for this catalytic behaviour: evidence for some Pd redispersion were found by XRD.¹⁵ However, the small CO/Pd values measured over the two systems suggest similar Pd exposed area, particularly when compared to the fresh sample. Both TPR profiles and H₂ chemisorption showed much more efficient low temperature H₂ activation and spillover in the PdCZ Aged-Ox compared to PdCZ Aged-Cyc. This cannot be associated with a simple Pd redispersion effect, but, as indicated by the HREM, CO-OSC and TPR studies,

by a simultaneous occurrence of chemical and nano-structural changes affecting both the metal phase and, particularly, the mixed oxide support. CeO_2 -ZrO₂ supports play a key role in these phenomena.^{11,12}

In summary, the observed critical importance of the ageing/ reactivation conditions, and, particularly, of the high temperature oxidation, in maintaining high catalytic efficiency of these Pd-CZ materials is relevant not only to TWCs but may also suggest novel strategies for development of efficient and durable catalytic systems for reactions related to on-board H₂ production from fuels, *e.g.* fuel-reforming and WGSR, where catalyst deactivation is an important issue.¹⁶

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